

Simulation of an Impulse Arc Discharge in Line Lightning Protection Devices.

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Introduction: Impulse arc discharge in Line Lightning Protection Device (LLPD) triggered by lightning overvoltage is

Results: Preliminary simulation results allow to evaluate the influence of chamber geometry on arc decay rate.

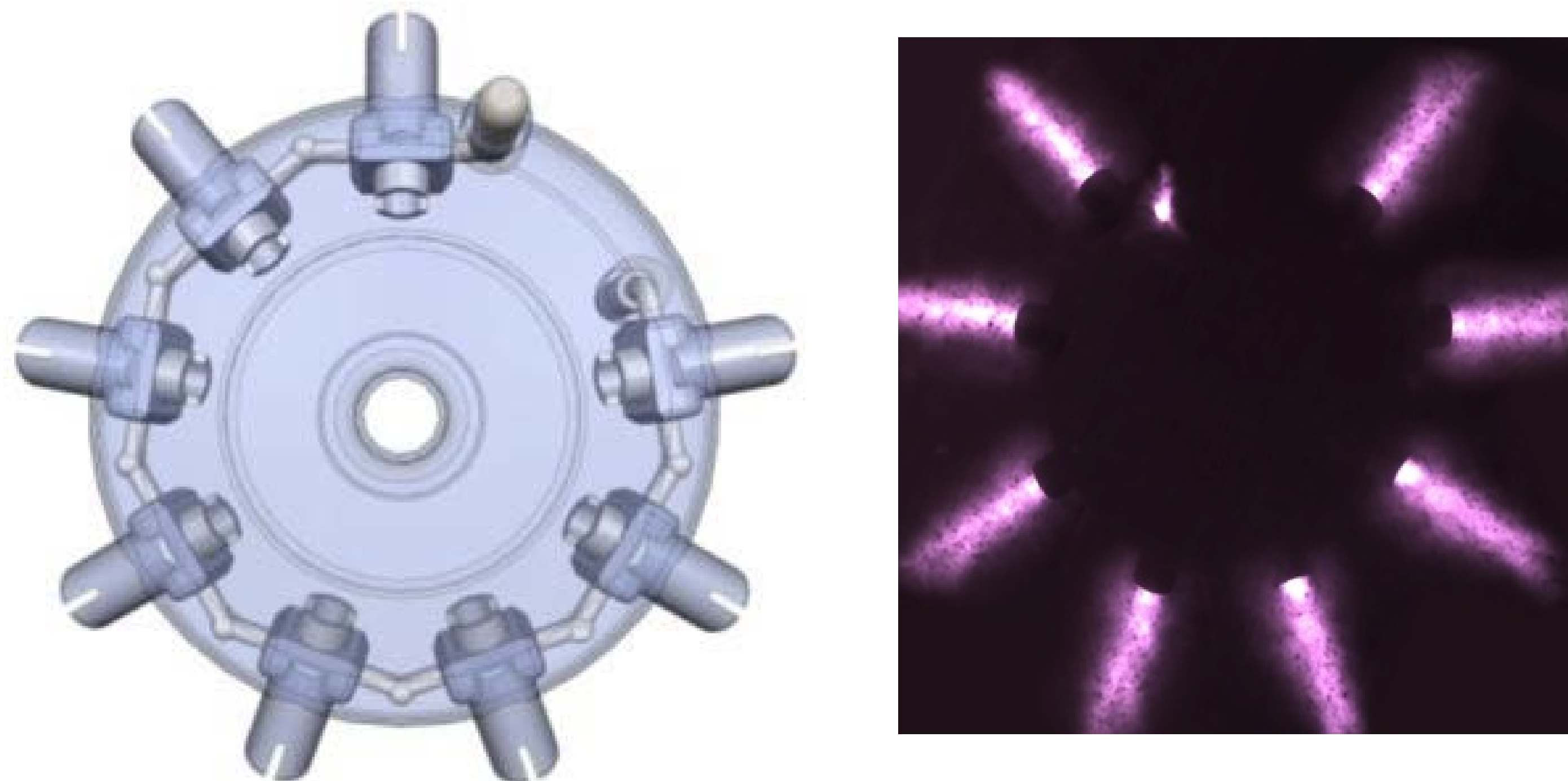


Figure 1. LLPD CAD model and real sample in operation mode

Computational Methods: Set of magnetohydrodynamic (MHD) equations is applied to describe arc discharge behavior during lightning current pulse impact. Coupling of CFD and ACDC modules was implemented.

$$\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \mathbf{u}) = 0$$

$$\frac{\partial(\rho \mathbf{u})}{\partial t} + \nabla \cdot (\rho \mathbf{u} \otimes \mathbf{u}) = -\nabla p + \nabla \cdot \hat{\boldsymbol{\tau}} + [\mathbf{j} \times \mathbf{B}]$$

$$\frac{\partial(\rho h)}{\partial t} + \nabla \cdot (\rho h \mathbf{u}) = \frac{\partial p}{\partial t} + \nabla \cdot (\hat{\boldsymbol{\tau}} \mathbf{u}) + \mathbf{j} \cdot \mathbf{E} + \nabla \cdot (\mathbf{q}_{cond} + \mathbf{q}_{rad})$$

Terminal and Ground conditions are applied to corresponding electrodes. The boundary of air domain is set as Outlet.

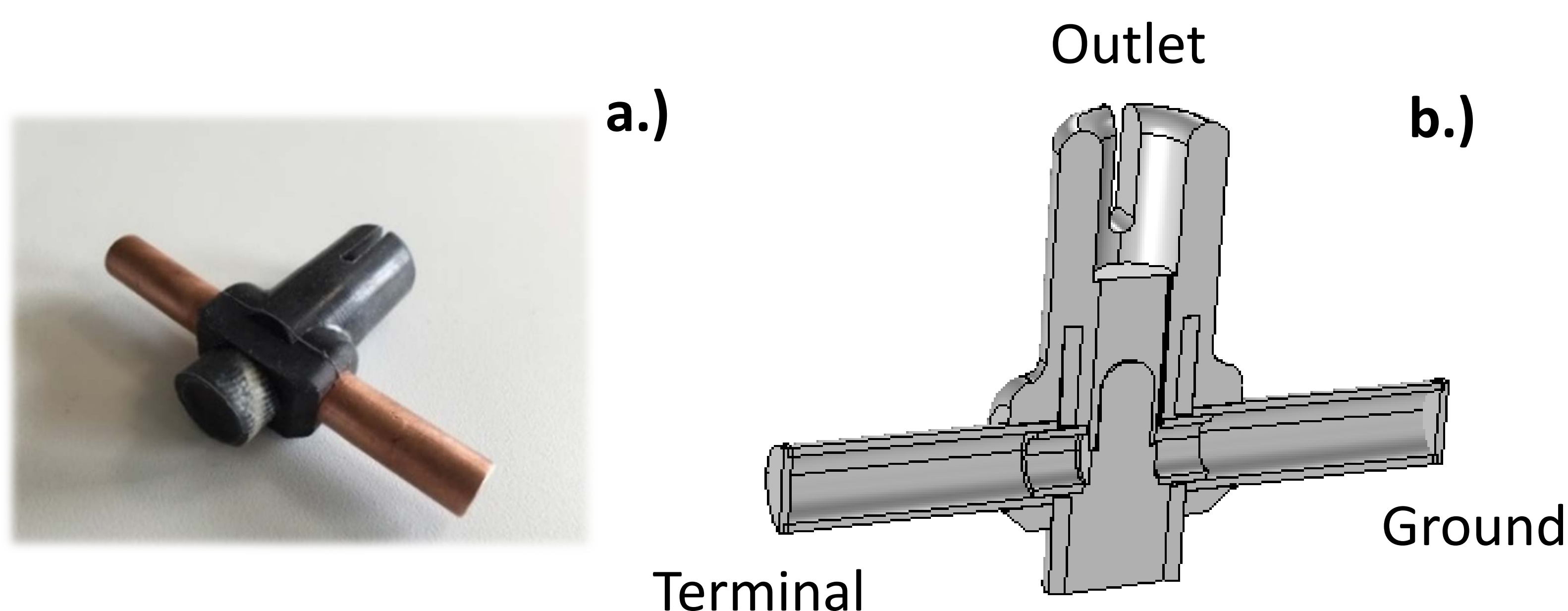


Figure 2. Discharge chamber: a.) Real-size sample b.) Computational domain

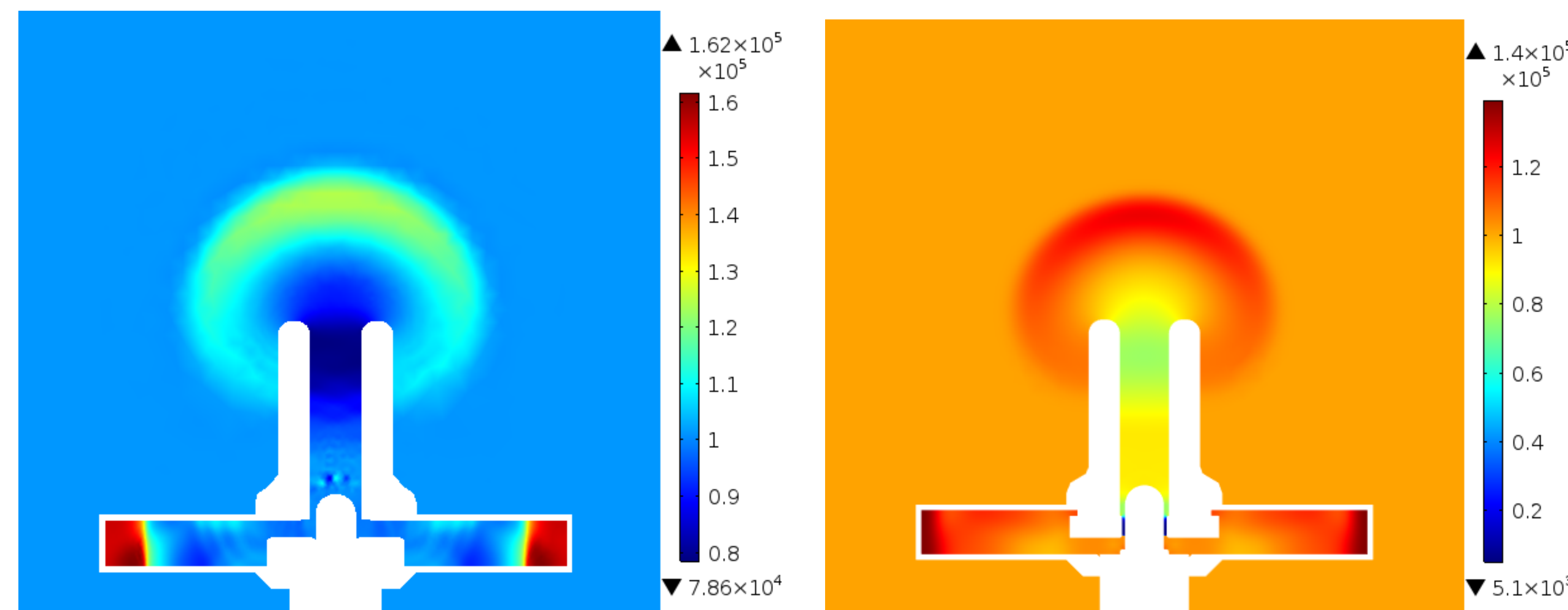


Figure 3. Pressure distribution

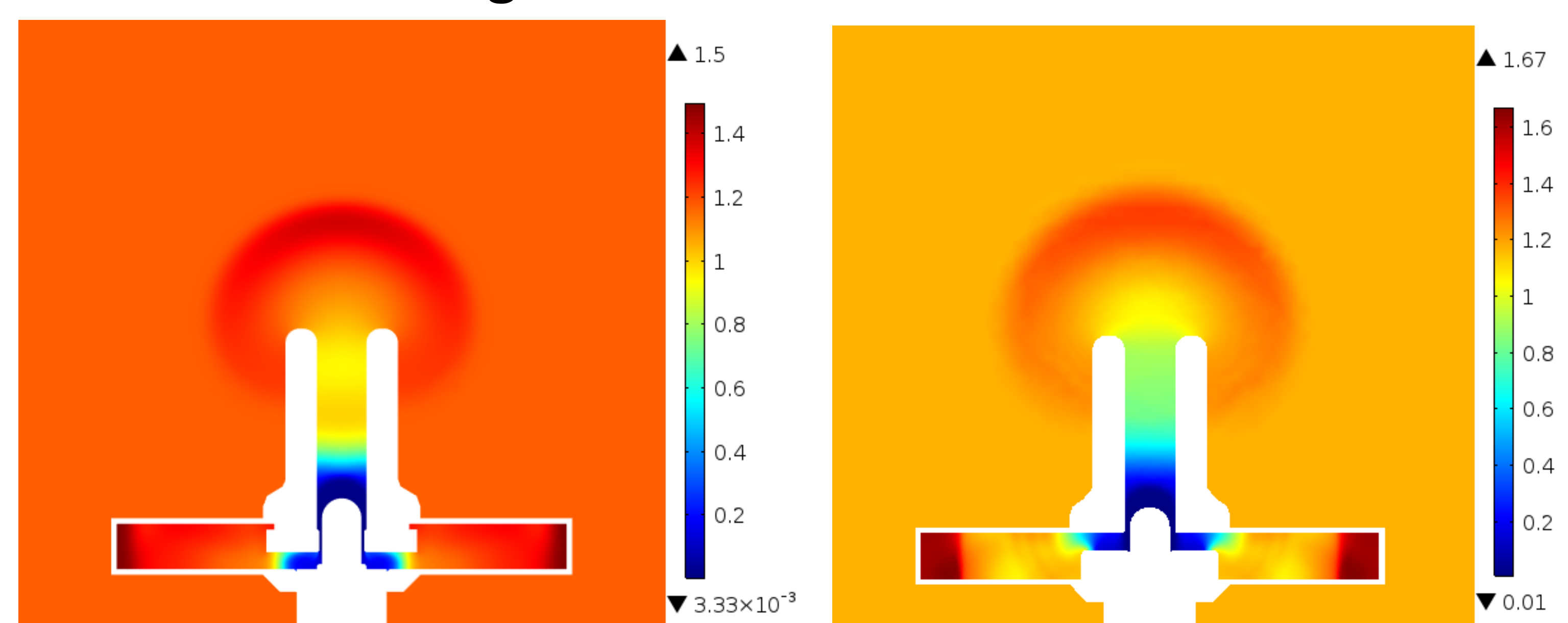


Figure 4. Density distribution

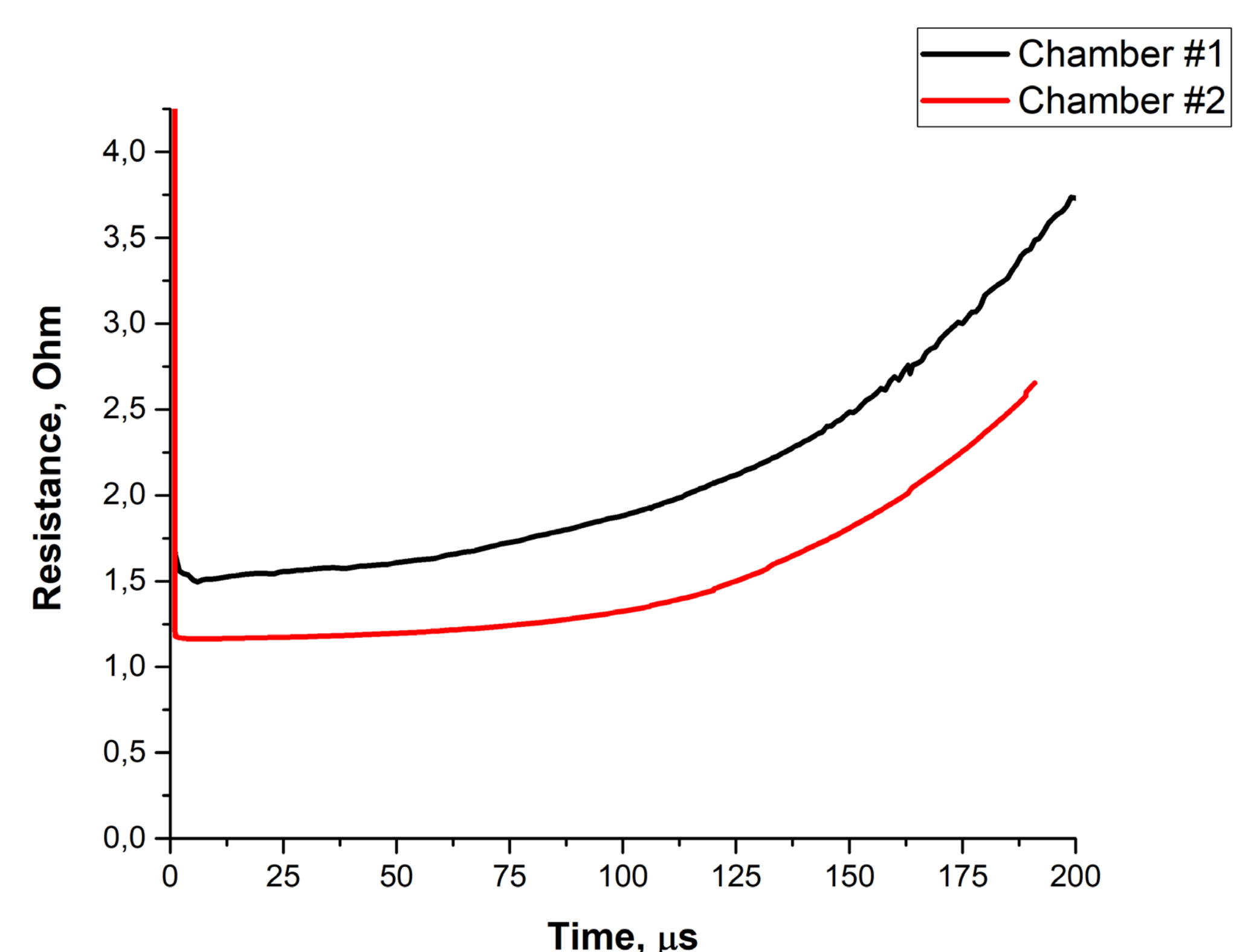


Figure 5. Resistance time dependence for two chamber designs.

Conclusions: Current state of simulations gives qualitative agreement with experimental data.

References:

1. G.V.Podporkin, Overhead lines lightning protection by multi-chamber arrestors and insulator-arrestors, IEEE Transaction on Power Delivery, 1,26(1), 214-221, (2010)
2. H.Nordborg, Modeling and simulation of the current quenching behavior of line lightning protection device, Journal of Physics D: Applied Physics, 50, (2017)