-EPFOOP-

Prof. Mario Paolone, DESL, Distributed Electrical Systems Laboratory
Nicolò Riva, SCI IC BD - Applied Superconductivity
Zsófia Sajó, M.Sc. Student in Materials Science and Engineering
Dr. Lorenzo Benedetti, GEL - GeoEnergy Laboratory, ENAC



Outline

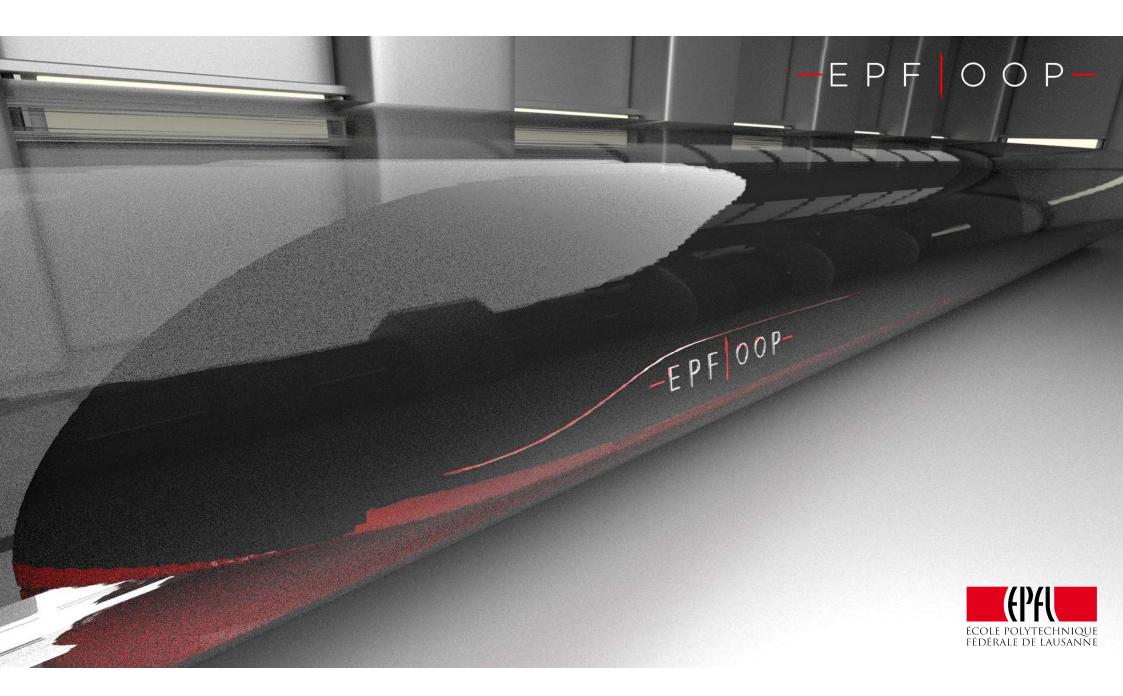
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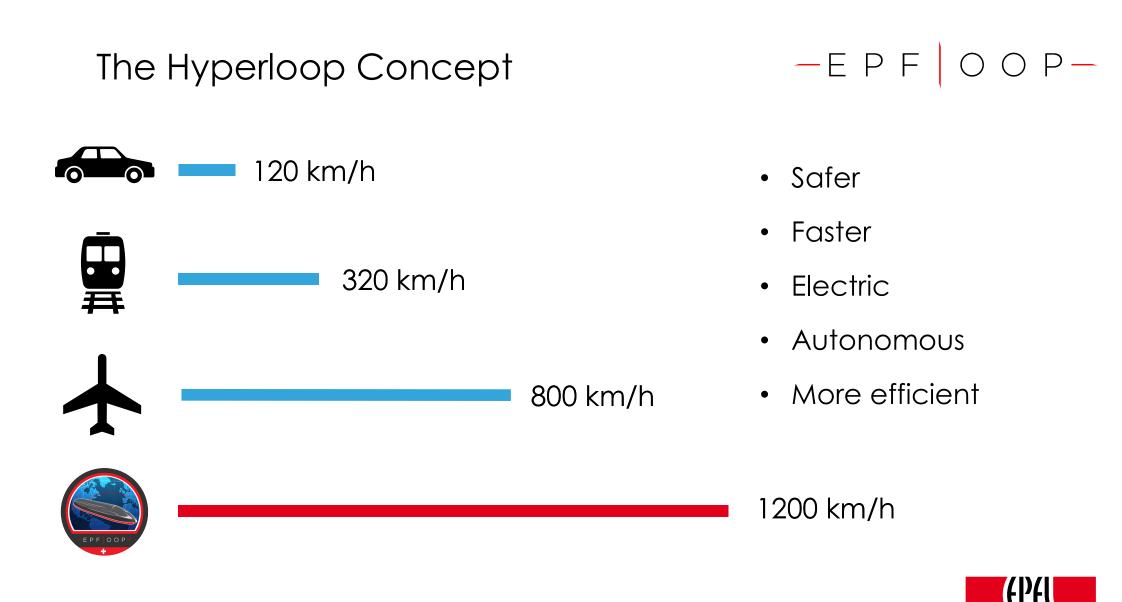
- The Hyperloop Concept
- The Competition 2018 Team, Design and Achievements
- Modeling of the 2018 Design
 - CFD
 - Structural
 - Thermal
- Future the 2019 Design



THE HYPERLOOP CONCEPT







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The Hyperloop Concept

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Technical Challenges

-EPF OOP-

Define a design targeting an optimal power/mass ratio

Mechanical Energy

Define the propulsion system capable of providing the best acceleration



Design pressurized systems capable of maintaining atmospheric pressure in the vacuum tube



Optimal/safe design of a battery energy storage system operating for high current discharge





Design a real-time and fault-tolerant autopilot



Mechanical

Software

Aerodynamics

Design and manufacture all the sub-components of the vehicle



THE TEAM -epf|00p-

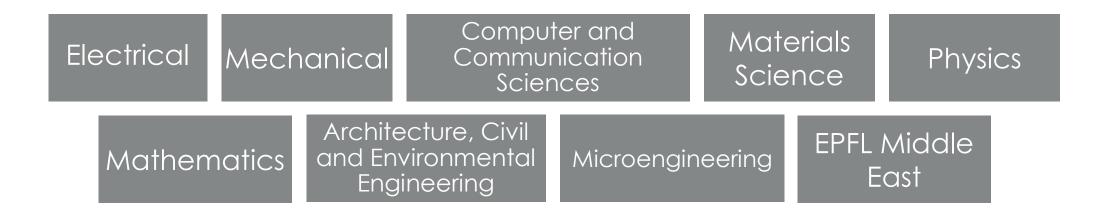




Team Structure

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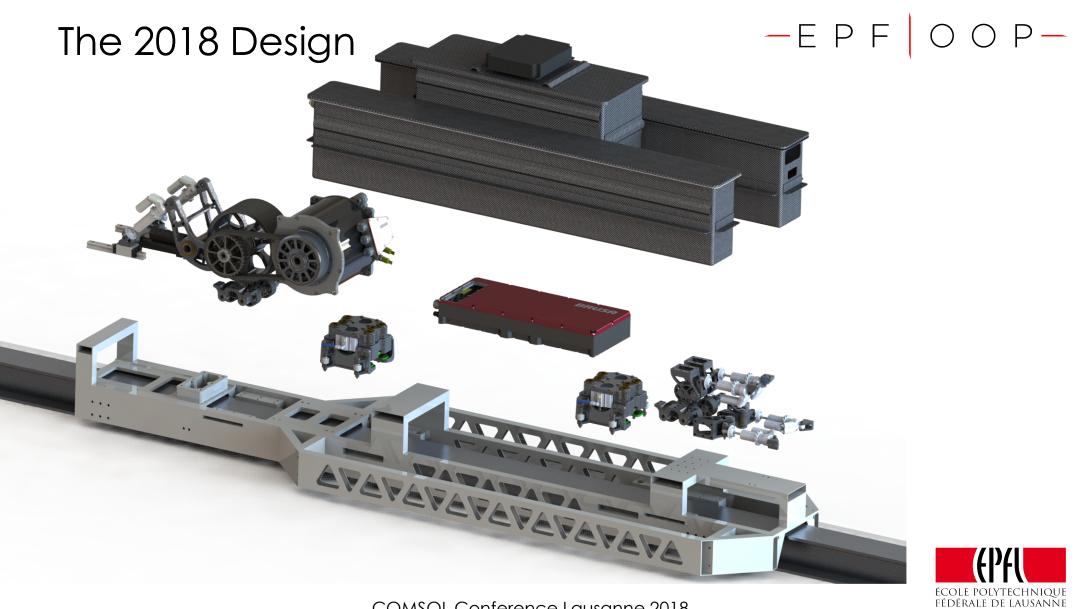
9 different EPFL sections involved





THE 2018 DESIGN - E P F | 0 0 P-





ACHIEVEMENTS AT THE 2018 COMPETITION - E P F | O O P -





Achievements

-EPFOOP-

1ST PLACE FOR THE DESIGN - HIGHEST RANKING FOR POD ENGINEERING

- 1ST PLACE IN SWITZERLAND
- TOP 3 HYPERLOOP TEAMS IN THE WORLD

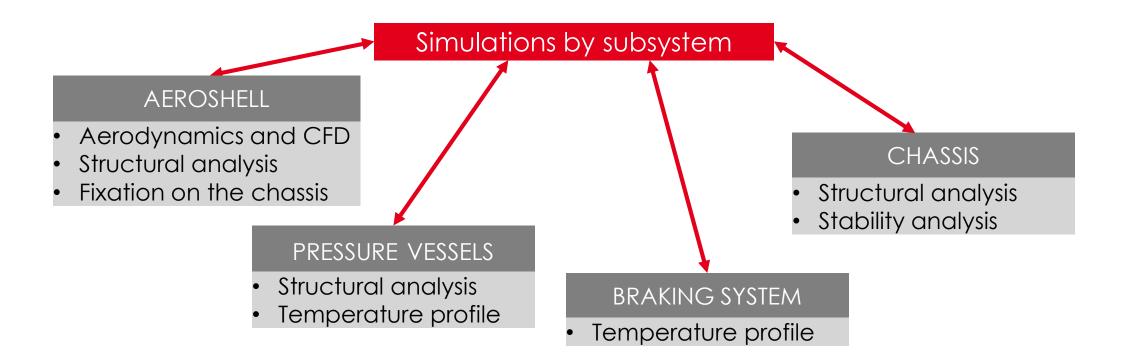
Feedback from SpaceX

Very clean design. Great test data. Good answers for everything.

Incredibly well engineered, the best we have seen yet. Extreme attention to detail such as routing of battery. Very good brake design. Thorough testing before competition.

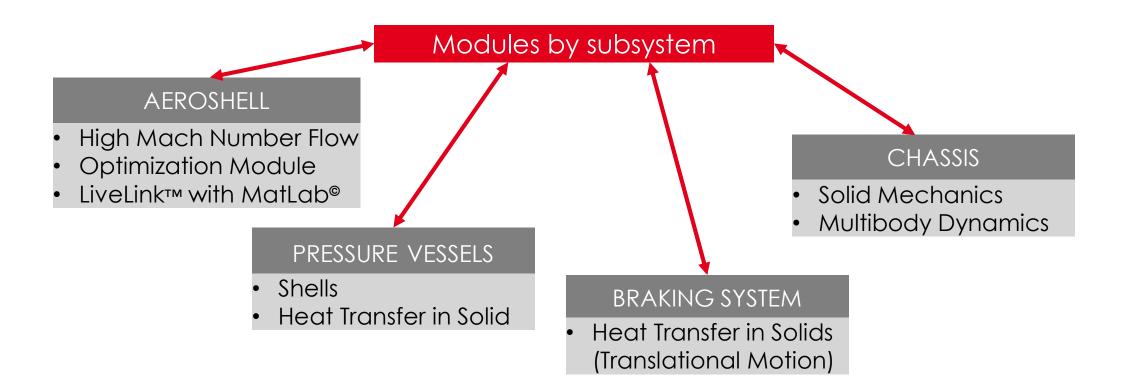


Subsystems Modelled with $COMSOL^{\mathbb{B}} - E P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P + P F | O O$



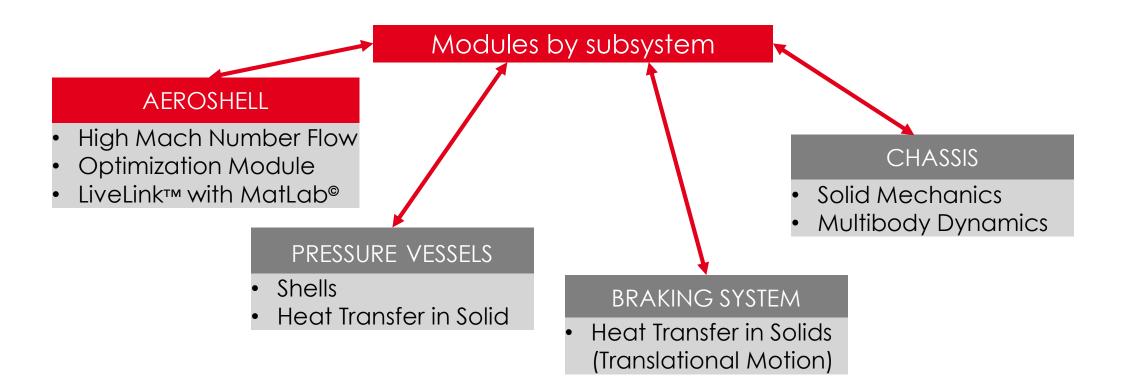


Subsystems Modelled with $COMSOL^{\mathbb{B}} - E P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P F | O O P - P + P F | O O$





Subsystems Modelled with $COMSOL^{\mathbb{B}} - E P F | O O P - P$





Aim of the Simulations

- The major interest in the design of the **aeroshell's shape** is to guarantee the **minimum aerodynamic resistance**
- The **optimization of the aeroshell's** shape is performed using CFD analysis
- The aeroshell should be both lightweight and withstand the applied loads (acceleration / deceleration and weight)
- A composite aeroshell was chosen and studied through structural analysis

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700

600

500

400

300

200

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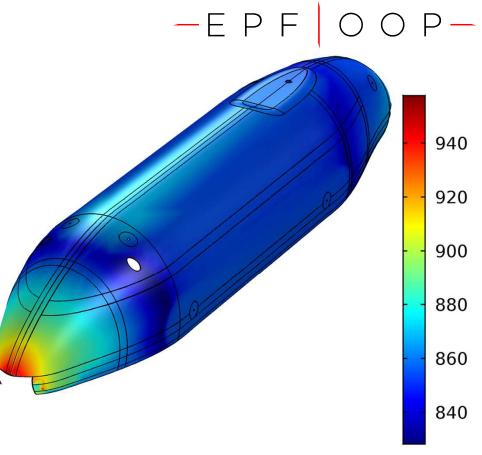
Modules, Solvers and Strategies

- CFD: The **High Mach Number Flow** functionality in stationary conditions, for evaluation of the **drag coefficient** and the **lift coefficient**
- Structural: **Shell** functionality in stationary conditions, for the arrangement of carbon fiber and epoxy, in sandwich structure with foam

Strategies

- Optimization through Genetic Algorithms and Optimization Module in 2D and validation in 3D
- Pressure load on the aeroshell surface
- Evaluation of the **safety factor**, adding more plies if needed

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Pressure distribution [Pa] obtained from CFD analysis and applied as load for the structural analysis

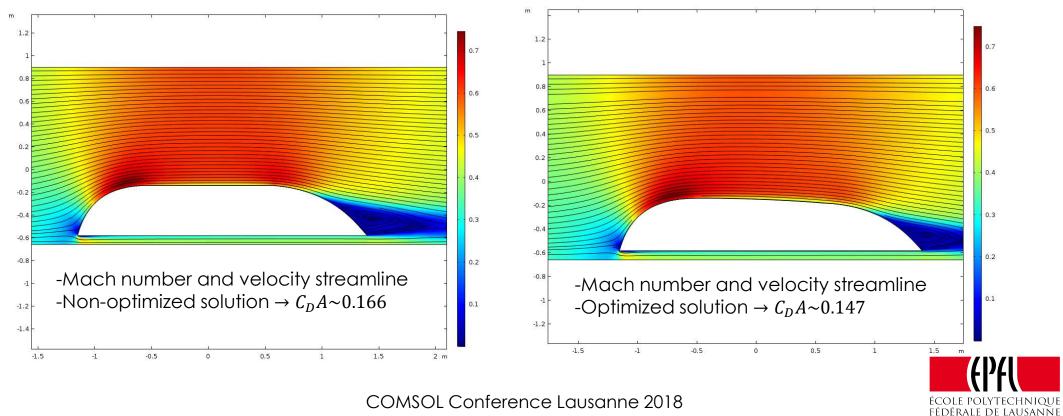


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- Study of the turbulent phenomena
- Drag and lift coefficients

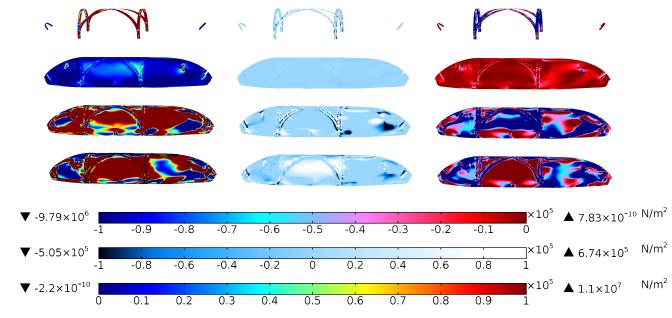
• Design optimization through LiveLink™ for MATLAB® and Optimization Module



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Results Structural Analysis

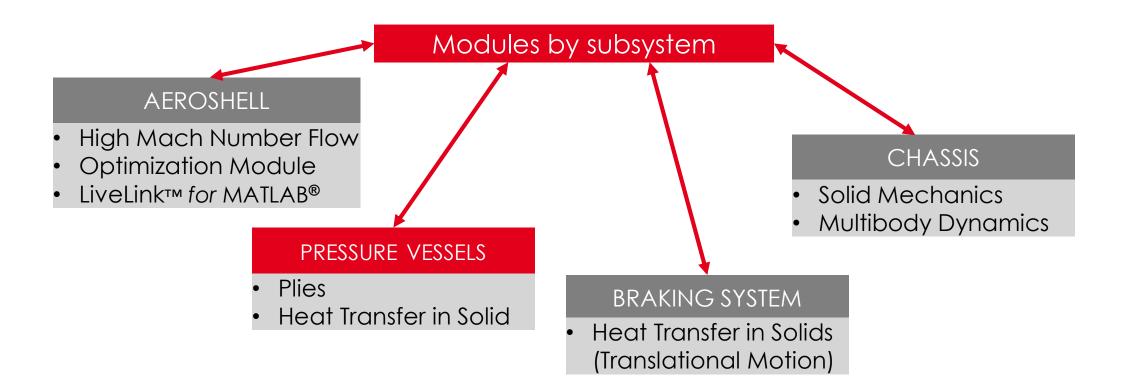
- Study of the mechanical loads applied on the shell
- Shells functionality used to simulate composite behaviour
- Pressure map obtained by the CFD simulations
- Acceleration / deceleration and weight loads
- Tsai-Wu safety factor and principal stresses were studied



Principal stresses 1, 2, 3 (left to right), inside to outside layers (top to bottom) (Pa)



Subsystems Modeled with $COMSOL^{\mathbb{B}}$ - E P F | O O P -





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Why Do We Need Them?

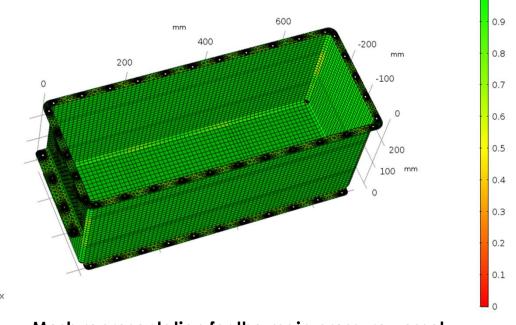
- The pressure vessels (PVs) are used to store electrical components in a pressurized environment (1 atm)
- The aim is to avoid a **direct exposure** of the components to the vacuum, which would be **destructive** for the batteries and the electronics inside





Aim of the Simulations

- The **carbon fiber composite** structure of the PVs should safely resist to the conditions in vacuum during the run
- In order to find the required set of plies, a **structural analysis** was performed
- The observed quantities have been the **Tsai**-**Wu safety factor** and the **principal stresses distribution**
- The goal is to ensure a **safety factor of 2** everywhere for the nominal loads (inner pressure and component inertia)



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Mesh representation for the main pressure vessel Mesh quality measured by skewness The main PV contains power and control electronics



O O P -

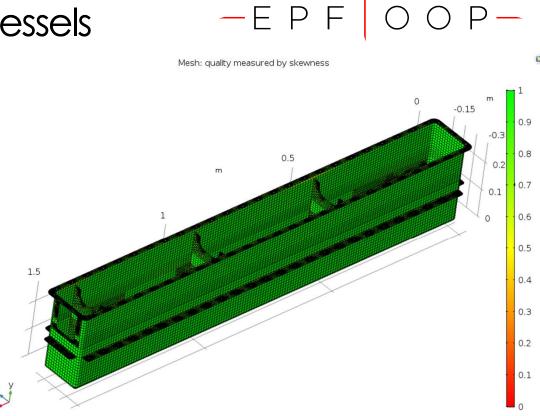
Modules, Solvers and Strategies

Module

 The Shells functionality has been used to simulate in stationary conditions the arrangement of plies of carbon fiber and epoxy composite, in sandwich structure with foam

Strategies

• A parametric sweep has been performed, varying the pressure load on the inner surfaces, in order to evaluate the safety factor for a range of pressures



Mesh representation for the lateral pressure vessel Mesh quality measured by skewness The lateral PVs contain mainly batteries



Results

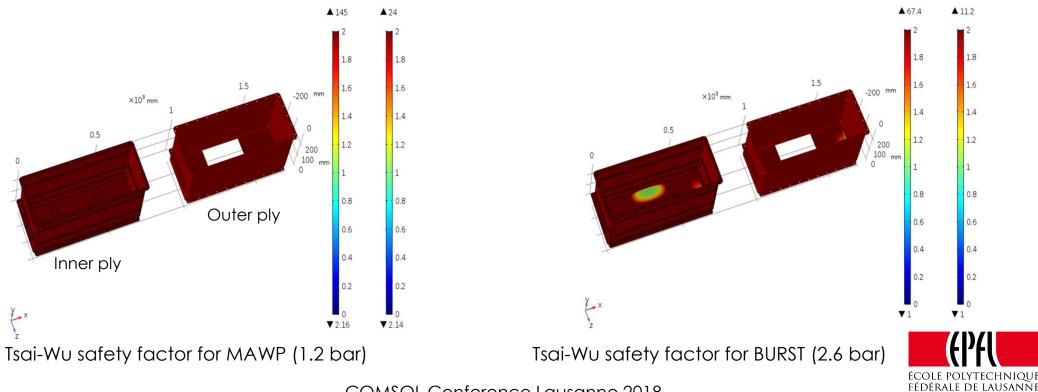
Iterative process: Reinforcing with more plies the areas with the highest stress •

-EPF

OP-

SpaceX parameters: ٠

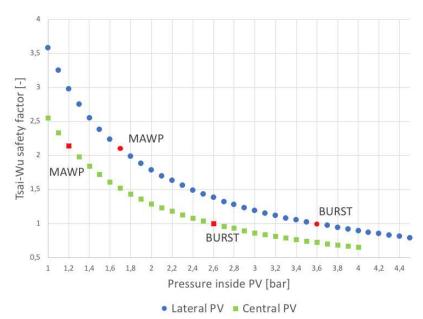
MAWP (Maximum Allowable Working Pressure – safety factor>2) BURST (safety factor<1)

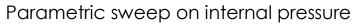


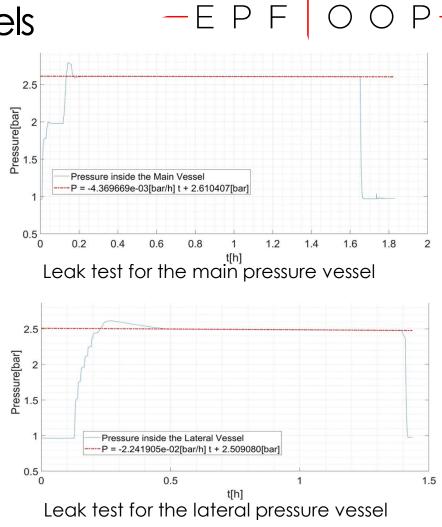
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Experimental Validation

- Compressed air was injected up to **1.6 bar**, to check the presence of leaks near **MAWP**
- Remarkably low leakages were observed (<20 mbar/h for all the PVs)

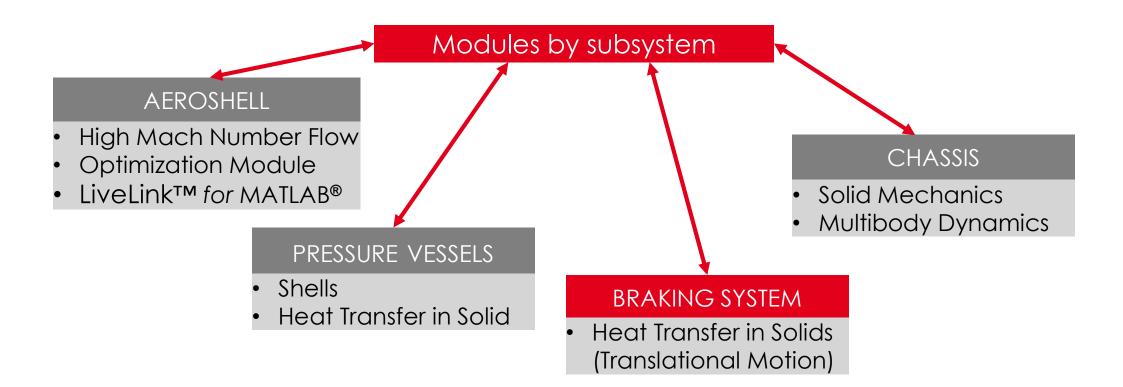








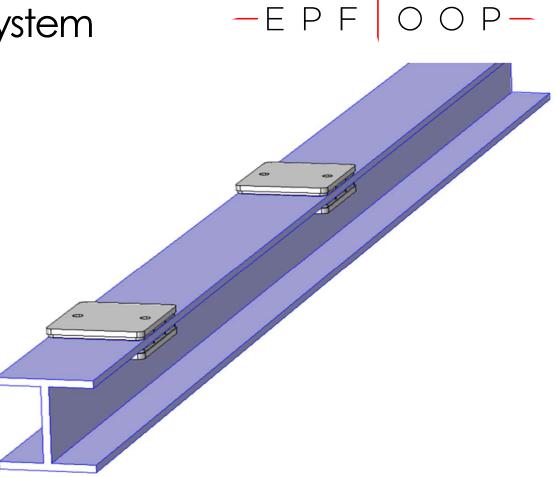
Subsystems Modeled with $COMSOL^{\mathbb{B}} - E P F | O O P - P$





Aim of the Simulations

- In order to stop safely after having reached top speed, it is required to have an efficient braking system
- The amount of **kinetic energy** carried by the pod can create an excessive **increase of temperature** in the brakes
- In order to choose the material constituting the brakes in order to avoid reaching problematic temperatures, simulations with heat transfer and frictional effects were performed





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Modules, Solvers and Strategies

Module

• The **Heat Transfer in Solid** module has been used to simulate the temperature profile behavior of the brakes during the braking at the end of the run

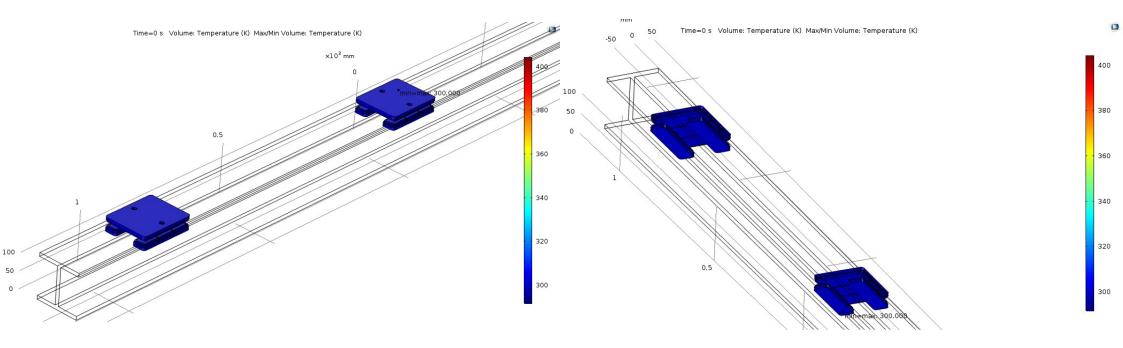
Strategies

 Using the Translation Motion and inserting the deceleration profile speed, it has been possible to estimate the power dissipated by friction on the rail and therefore the temperature rise in the pad volume



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Results



Temperature profile in the braking pads during the braking : material sweep

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Femperature (degC)

Results 550 Switch 1=Leather, Maximum: dset7 Switch 1=Organic pad, Maximum: dset7 Switch 1=Thermoplastic Polyurethane (TPUR), BASF, Maximum: dset7 500 Switch 1=Phenol Formaldehyde, Maximum: dset7 Switch 1=Teflon, Maximum: dset7 450 Switch 1=Plaster (Sand Aggregate), Maximum: dset7 —— Switch 1=Talc, Maximum: dset7 Switch 1=Calcite, Maximum: dset7 400 Switch 1=Boron nitride ceramics, Maximum: dset7 Switch 1=CombatBN A Saint Gobain, Maximum: dset7 350 Switch 1=Schunk Carbon Graphite -FH82A, Maximum: dset7 Switch 1=Polybutadiene, Maximum: dset7 300 250 200 150 100 50 2 6 10 Time (s) 12 14 16 18 20 0 4 8

Temperature profile in the braking pads during the braking : material sweep

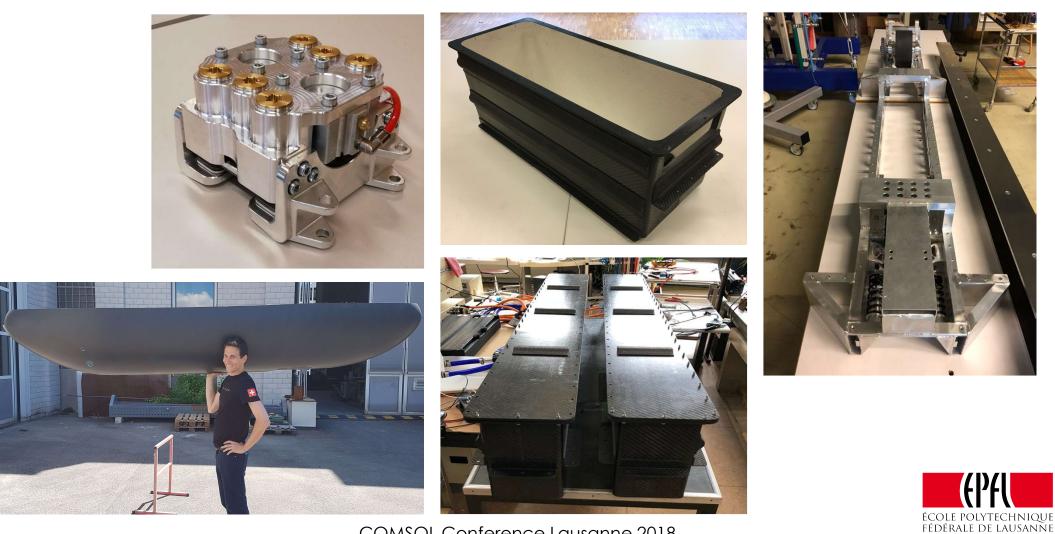
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The Manufacturing of the Pod

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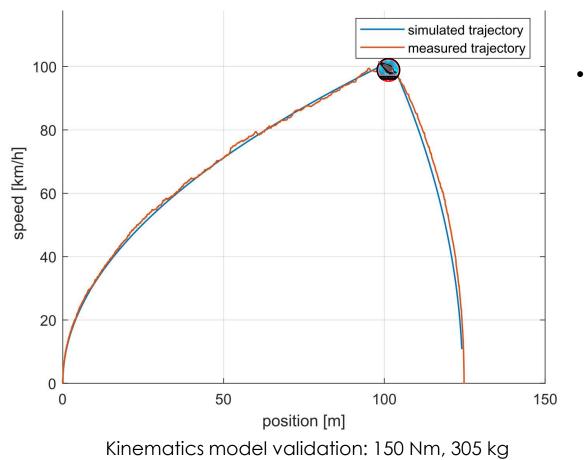
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Validation 0-100 km/h run used for the pod kinetic model validation

20.07.18

Pod Performances Validation

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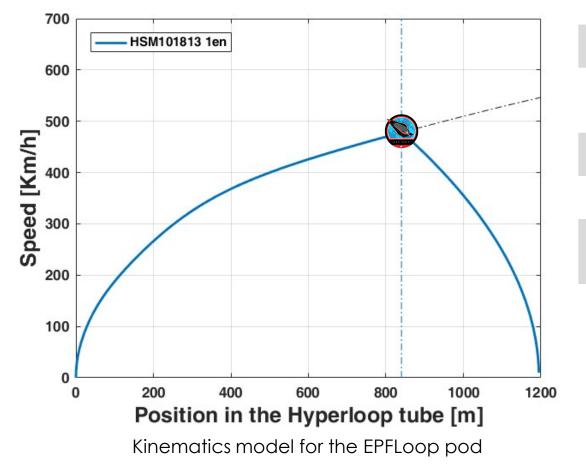


Comparison between the kinematics
 model developed by EPFLoop and
 measurements during the run



Pod Performances Prediction

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Mass	295 kg
Max requested power	178 kW
Max torque	385 Nm
Total capacity	15 Ah
Estimated max speed	470 km/h



THE 2019 HYPERLOOP COMPETITION - E P F 0 0 P-

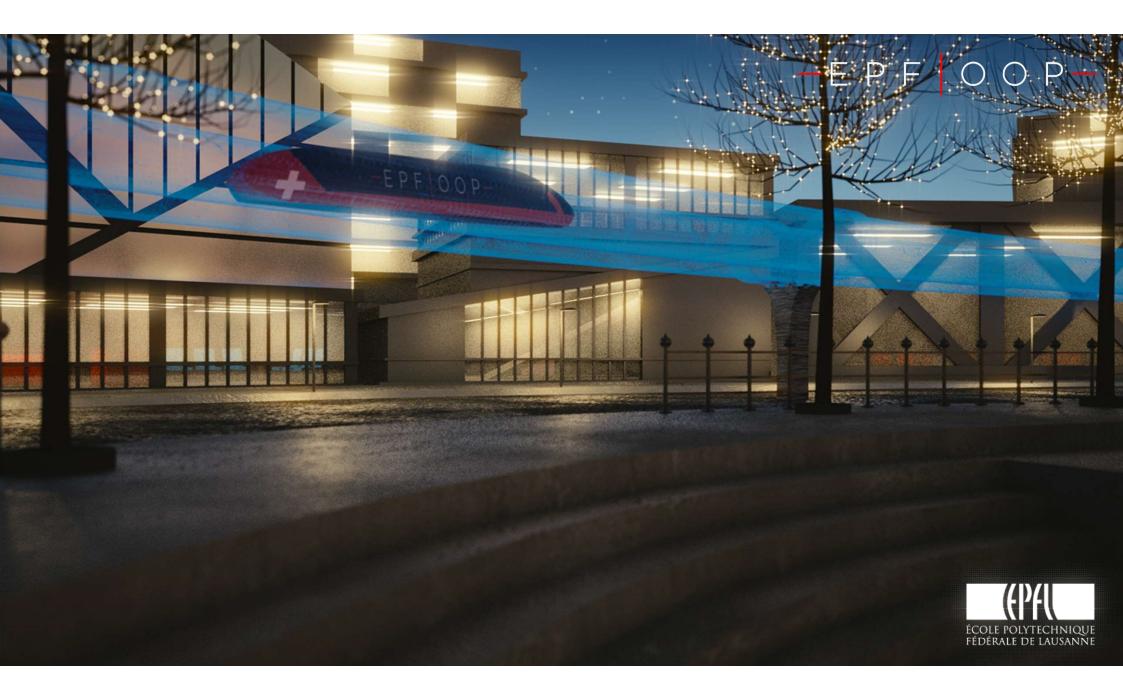


The 2019 Hyperloop Competition

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Increase maximum speed
 Scalable prototype
 New approach inspired by Swissmetro
 Optimal design
 Collaboration with partners such as COMSOL
 New involved students







Our Sponsors

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PLATINUM



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GOLD AND SILVER

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Special Thanks

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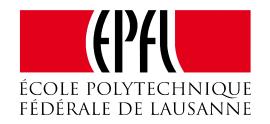
We would like to thank

Sven Friedel Alyona Friedel Thierry Luthy COMSOL (amazing!) Support



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