

# 2D Flow Past a Confined Circular Cylinder with Sinusoidal Ridges

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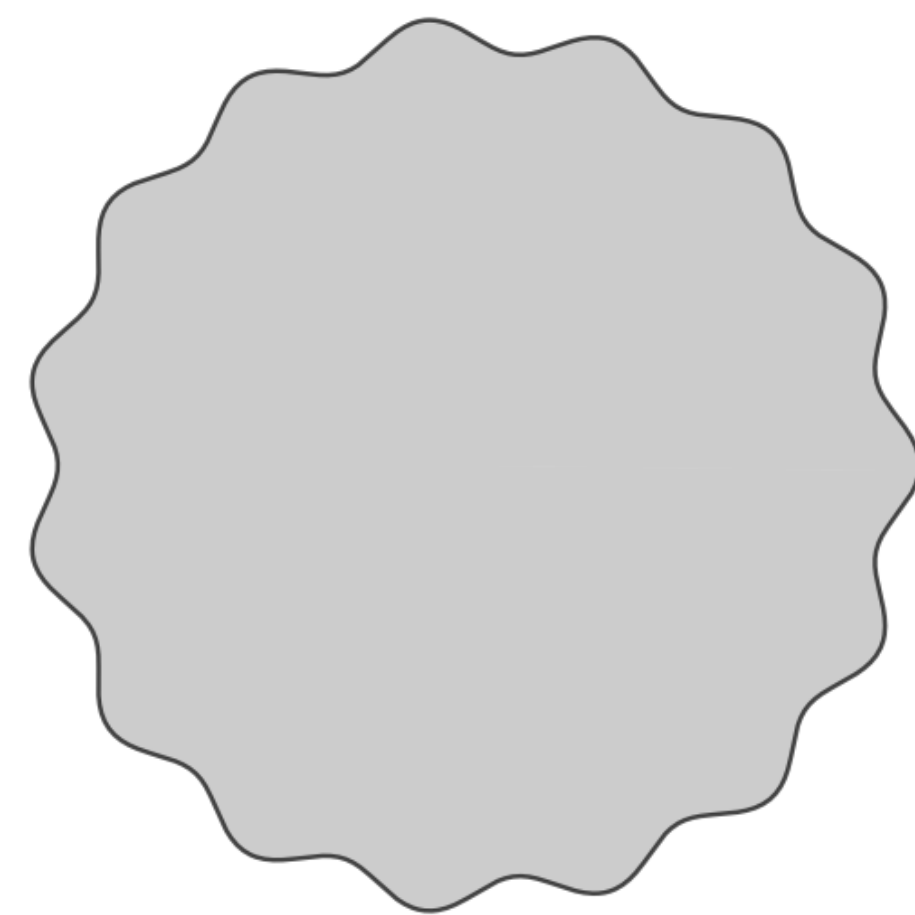
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**INTRODUCTION:** Using the CFD Module of COMSOL Multiphysics 5.4, we studied the flow past a circular cylinder with sinusoidal ridges (shown below), at Reynolds numbers of 20, 50, 200, and 500.

We define the cylinder in polar coordinates by

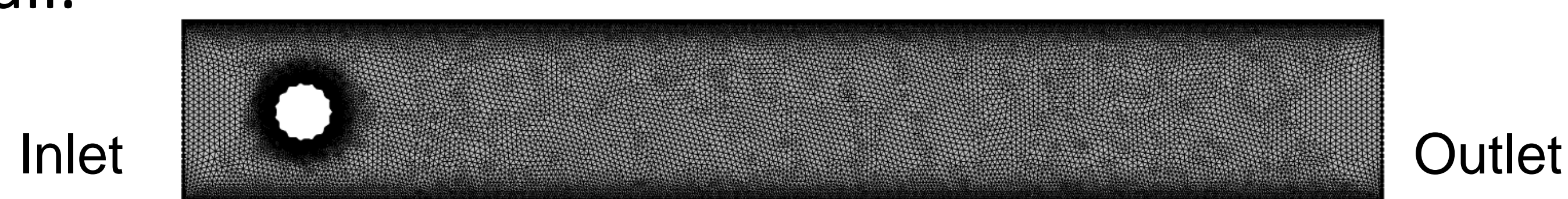
$$r(\theta) = \frac{L}{2} + a \cdot \cos(\omega\theta), \quad 0 \leq \theta \leq 2\pi$$

Where  $L = 0.15\text{m}$  is the base cylinder diameter,  $a$  is the ridge amplitude, and  $\omega$  is the number of ridges.



**Figure 1.** Sinusoidally ridged cylinder,  $a = L/25$ ,  $\omega = 15$ .

**COMPUTATIONAL METHODS:** The computational domain is a two-dimensional plane channel with length  $20L$  and width  $3L$ . The center of the cylinder is positioned in the center of the channel, a distance  $2L$  from the inlet. An inlet velocity with a parabolic profile is chosen at the leftmost wall, and a zero-pressure outlet boundary condition is chosen at the rightmost wall.



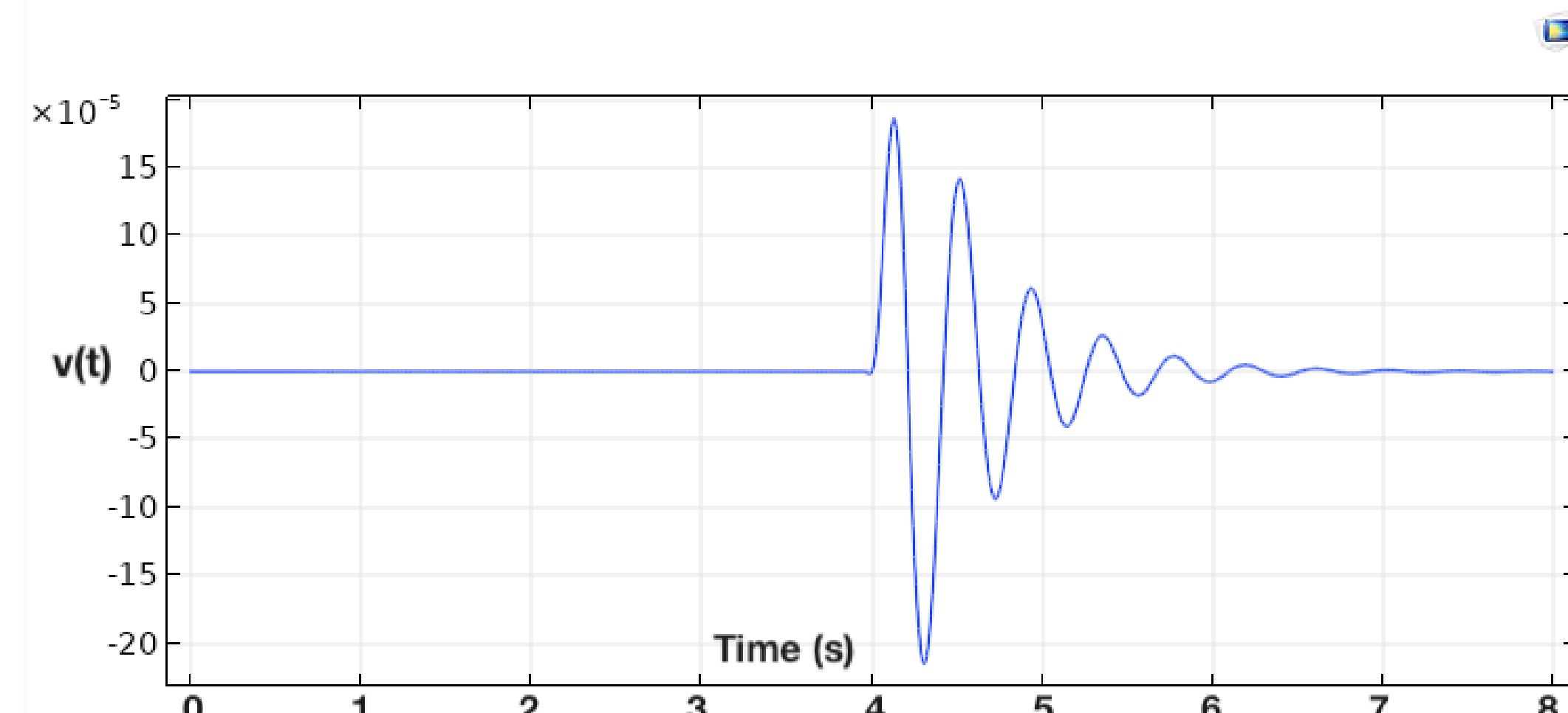
**Figure 2.** Computational domain with mesh

We use the following dimensionless quantities:

$$Re = \frac{\rho U_c L}{\mu}, \quad St = \frac{fL}{U_c}, \quad C_D = \frac{2F_D}{\rho U_c L}, \quad C_L = \frac{2F_L}{\rho U_c L}$$

Where  $U_c$  is the centerline velocity,  $f$  is the frequency of vortex shedding, and  $F_D$ ,  $F_L$  are the total drag and lift forces, respectively.

Additionally, we perturb the flow with a brief vertical oscillation of the cylinder in order to trigger vortex shedding at  $Re = 200$  and  $500$ .

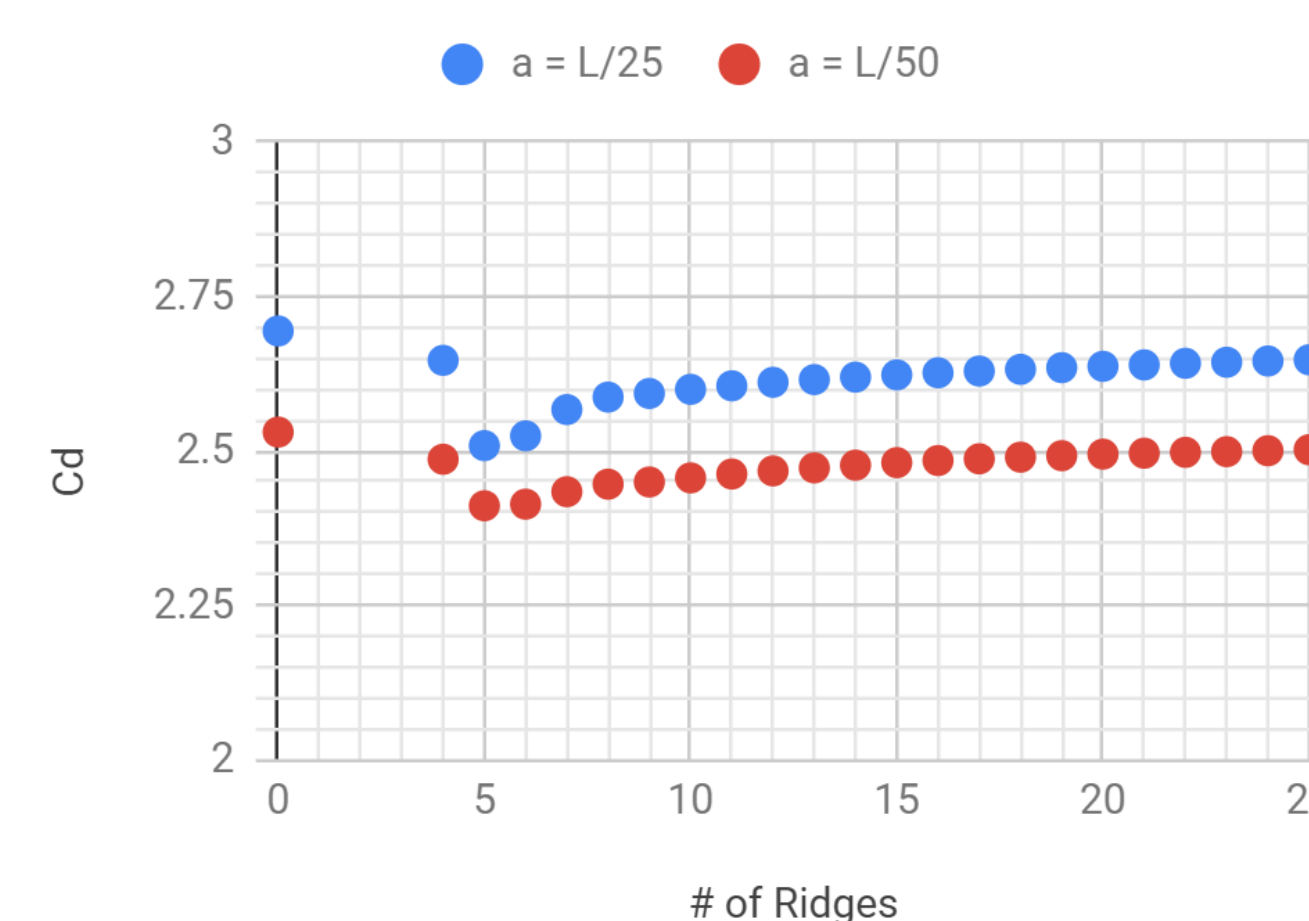


**Figure 2.** Perturbation velocity vs. time

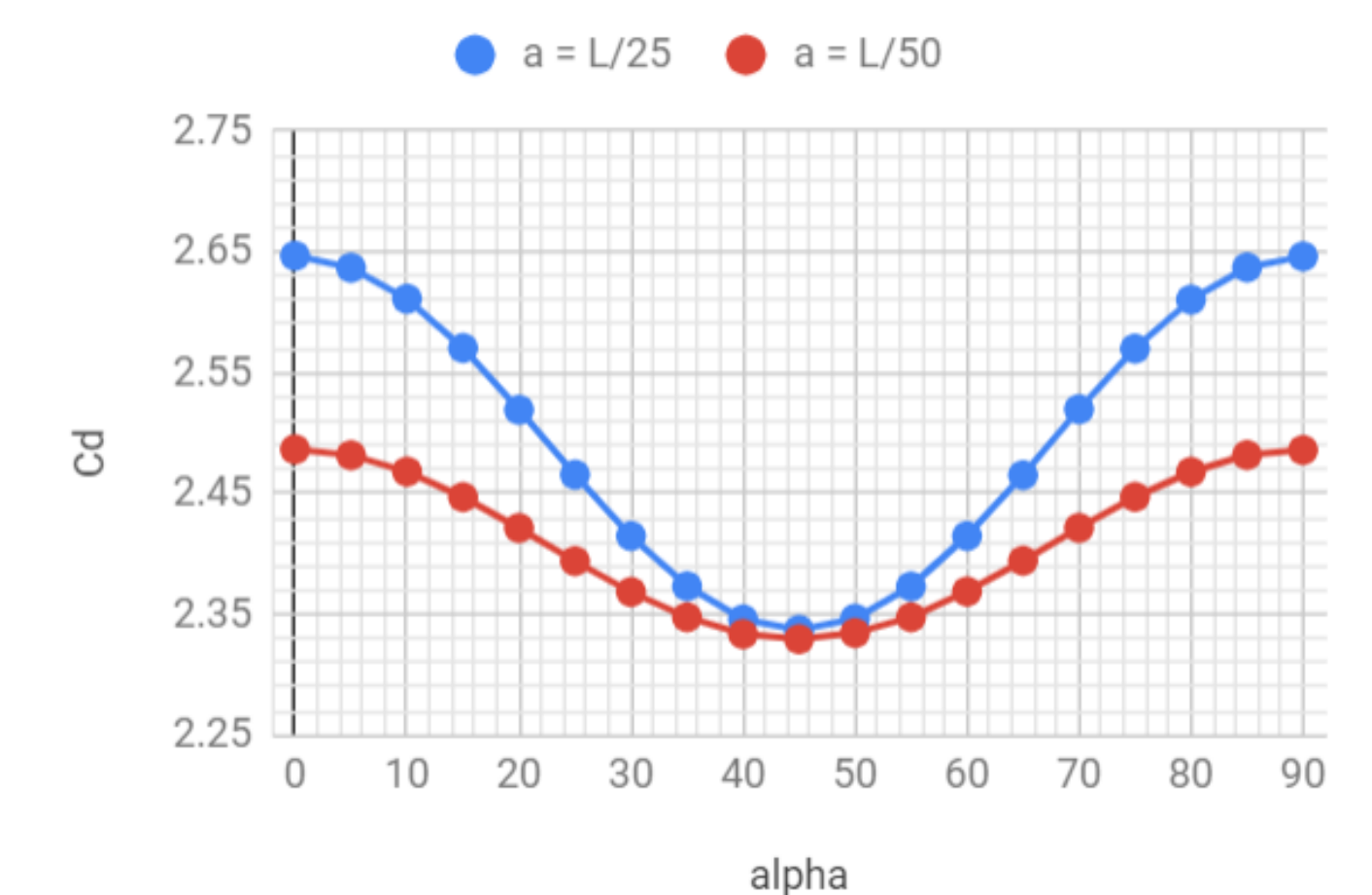
**VERIFICATION:** We check our results for a smooth cylinder against Schäfer et al (1996)[1] and Singha (2010)[2]. The results match with excellent agreement.

**RESULTS:** In the laminar flow regime, we found:

- The recirculation zone length is independent from the number of ridges
- The following relationships between the number of ridges and  $C_D$ , and for  $\omega = 4$ , between the counterclockwise angle of attack  $\alpha$  and  $C_D$ :



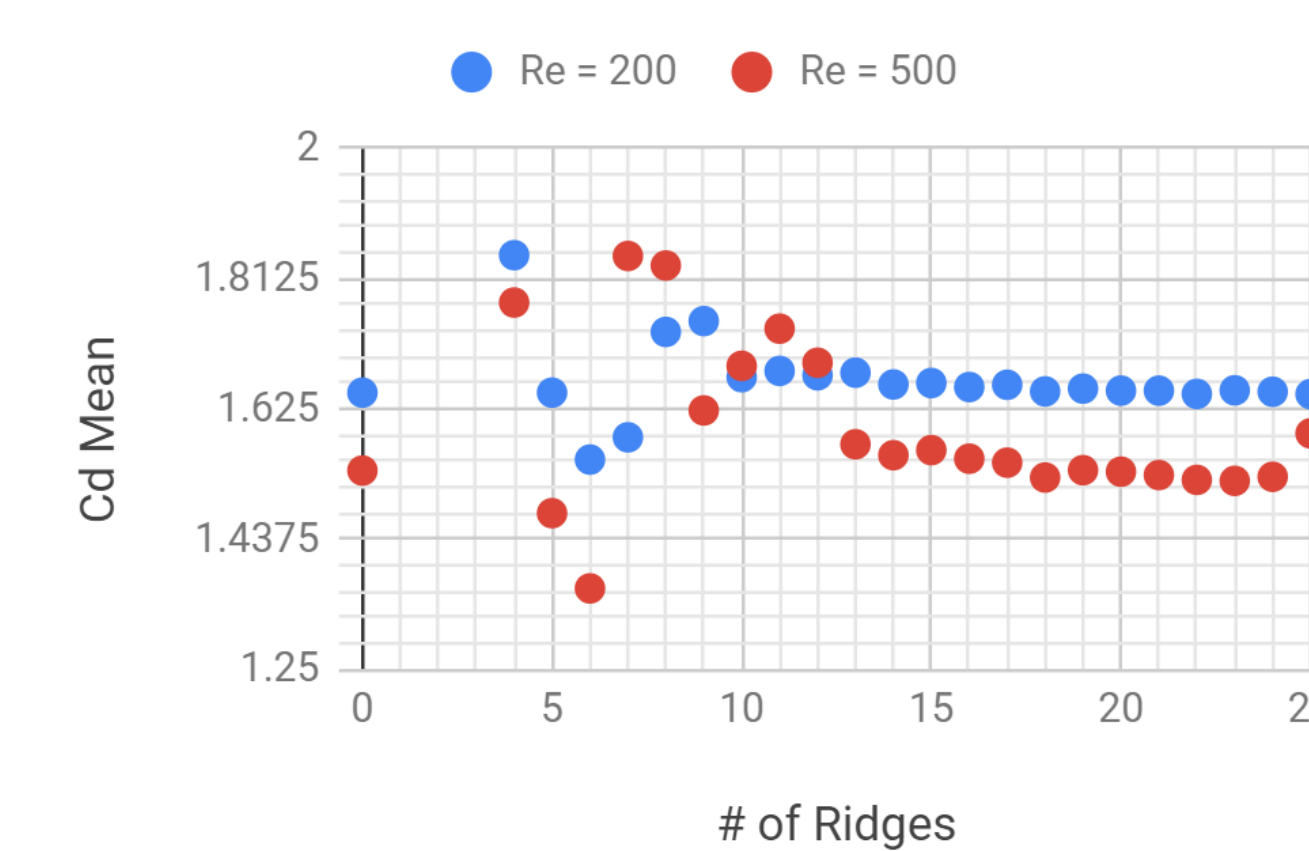
**Figure 3.**  $C_D$  vs.  $\omega$  ( $Re = 50$ )



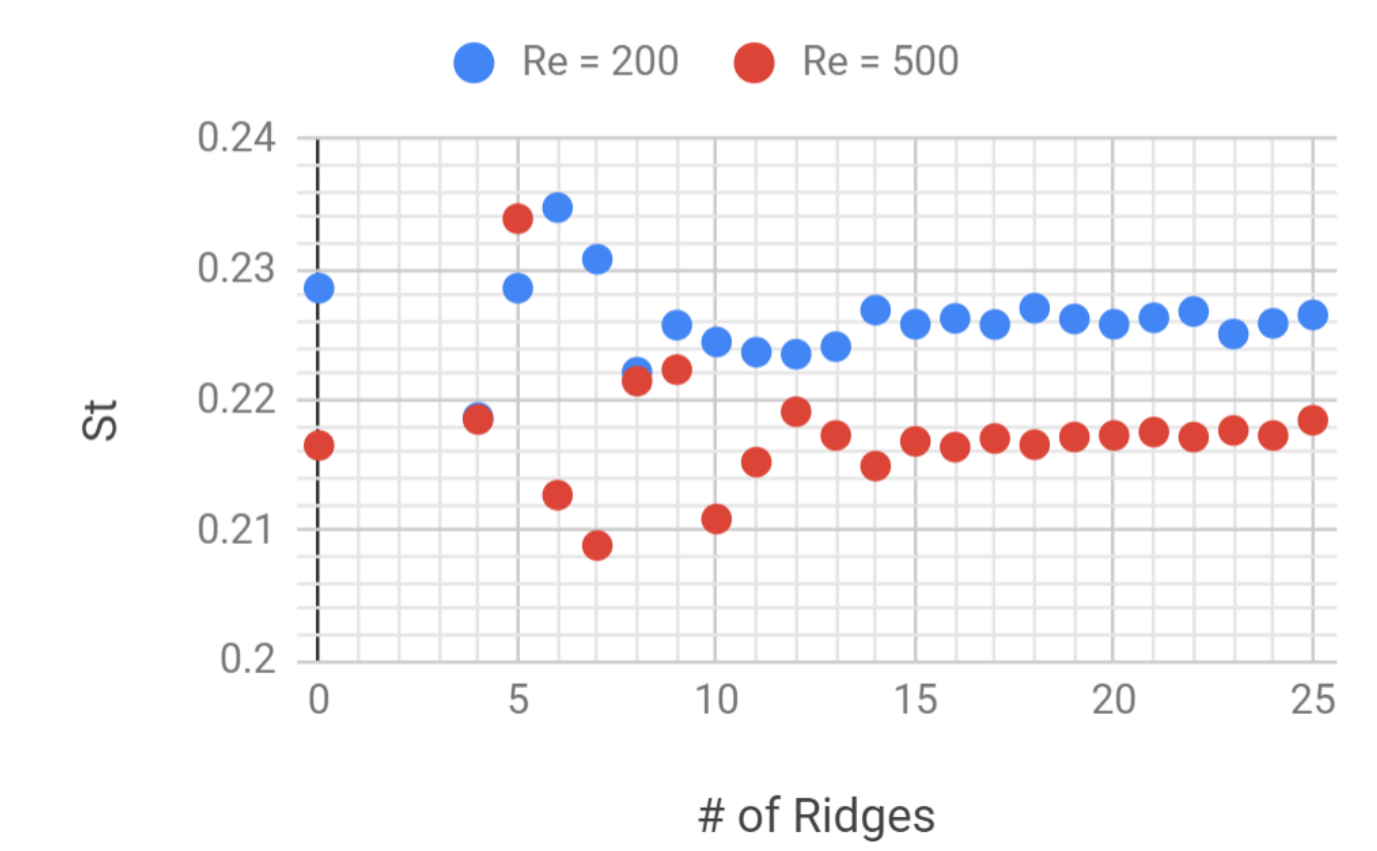
**Figure 4.**  $C_D$  vs.  $\alpha$  ( $Re = 50$ ,  $\omega = 4$ )

- Similar relationships were found for  $Re = 20$ .

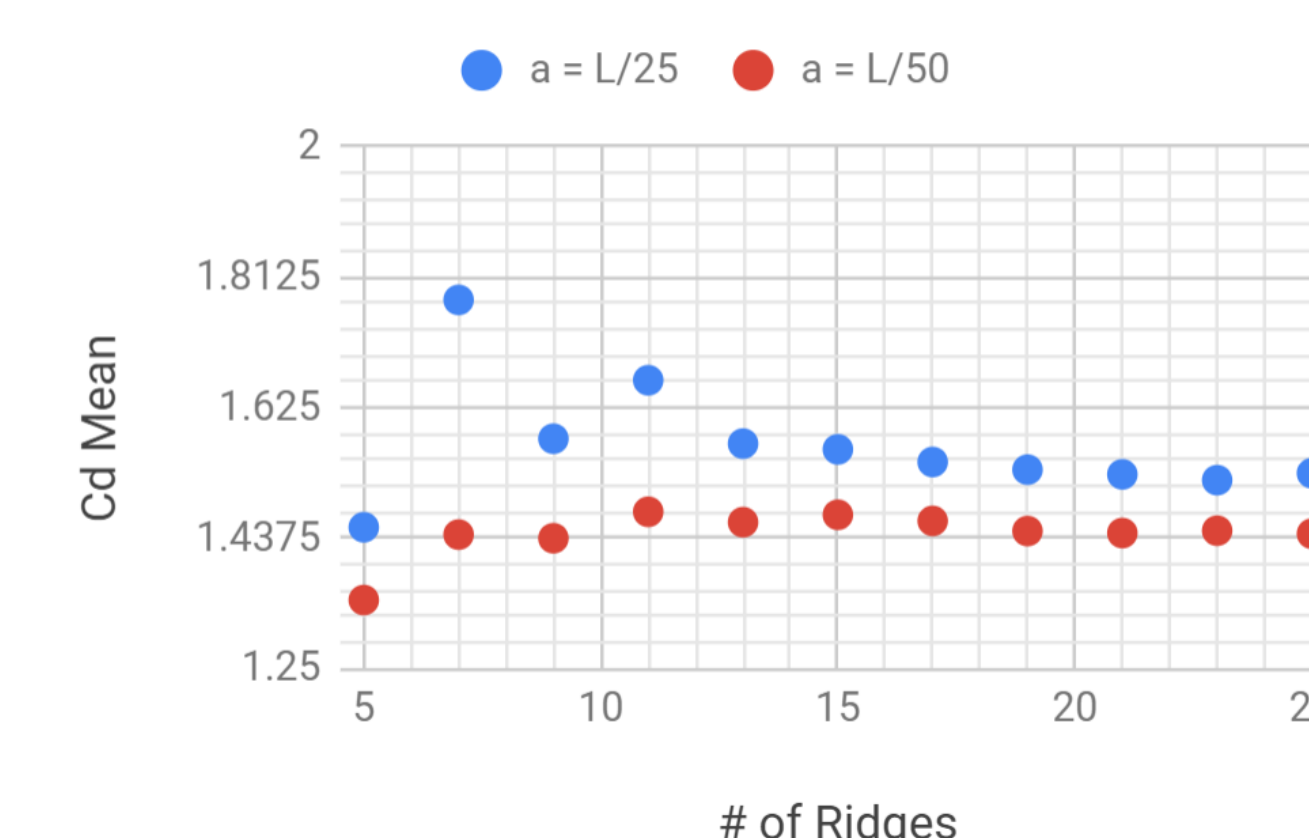
In the periodic shedding regime, we found the following relationships:



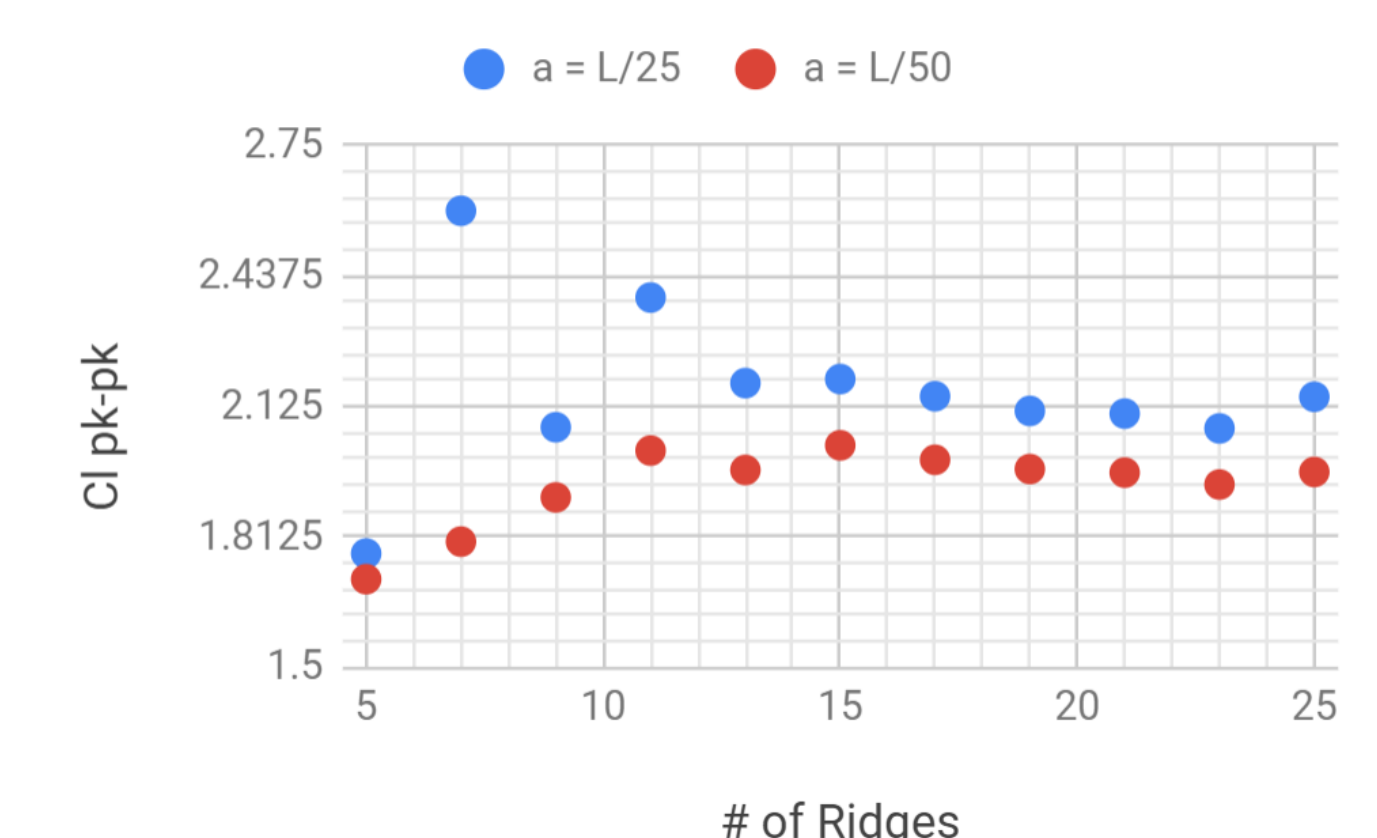
**Figure 5.**  $C_{D, \text{mean}}$  vs.  $\omega$ ,  $Re = 200$  and  $500$  ( $a = L/25$ )



**Figure 6.**  $St$  vs.  $\omega$ ,  $Re = 200$  and  $500$  ( $a = L/25$ )



**Figure 7.**  $C_{D, \text{mean}}$  vs.  $\omega$ ,  $a = L/25$  and  $a = L/50$  ( $Re = 500$ )



**Figure 8.**  $C_{L, \text{pkpk}}$  vs.  $\omega$ ,  $a = L/25$  and  $a = L/50$  ( $Re = 500$ )

- Values for the Strouhal number,  $St$ , were also computed.

**CONCLUSIONS & FURTHER RESEARCH:**

- As  $\omega$  increases, the  $C_D$ ,  $C_L$ , and  $St$  values tend to approach that of a smooth cylinder ( $\omega = 0$ ).
- When  $\omega > \sim 13$  in the periodic shedding regime, values for  $St$ ,  $C_{D, \text{mean}}$ , and  $C_{L, \text{pkpk}}$  become approximately steady. When  $\omega < \sim 13$ , results are erratic and no clear trend can be deduced.
- More research needs to be done to investigate the unique geometry of cylinders with  $1 \leq \omega \leq 4$ .

**REFERENCES:**

1. Schäfer, M. et al., Benchmark computations of laminar flow around a cylinder, *Flow simulation with high-performance computers II*, pp. 547-566. Springer Vieweg Verlag, Germany (1996)
2. Singha, S. and Sinhamahapatra, K. P., Flow past a circular cylinder between parallel walls at low Reynolds numbers, *Ocean Engineering*, **37**, No. 8-9, pp. 757-769 (2010)

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