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A 2D Axisymmetric Electrodeposition Model

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Introduction to Electrodeposition:

- **Widely Employed Technology**

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- Large Literature {1}

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- Nanotechnology
- etc.

This 2D Axisymmetric Electrodeposition Model:

- High Aspect-Ratio Well Plating

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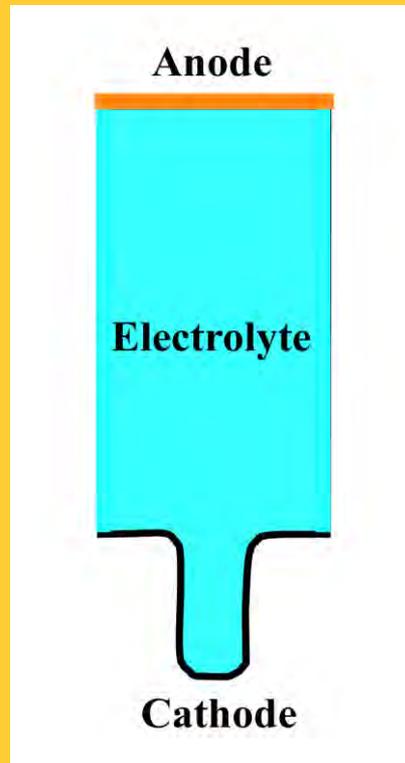
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- Based on Fick's Law {3} plus Electrostatic Forces

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This 2D Axisymmetric Electrodeposition Model:

Governing Processes: Nernst-Planck Equation

$$N_i = -D_i \nabla c_i - z_i u_i F c_i \nabla V$$

Where: N_i = mass transport vector [mol/(m²*s)]

D_i = Diffusivity of the i^{th} species in the electrolyte [m²/s]

c_i = Concentration of the i^{th} species in the electrolyte [mol/m³]

z_i = Charge of the i^{th} species in the electrolyte [1] (unitless)

u_i = Mobility of the i^{th} species in the electrolyte [(mol*m²)/(J*s)]

F = Faraday's constant [A*s/mol]

V = Potential in the fluid [V]

This 2D Axisymmetric Electrodeposition Model:

Governing Processes: Nernst-Planck Equation

The mobility u_i of the i^{th} species can be expressed as:

$$u_i = \frac{D_i}{RT}$$

Where: D_i = Diffusivity of the i^{th} species in the electrolyte [m^2/s]

R = Universal gas constant $8.31447[\text{J}/\text{mol}\cdot\text{K}]$

T = Temperature [K]



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Governing Processes: Nernst-Planck Equation

The material balances for each species are expressed as:

$$\frac{\partial c_i}{\partial t} = -\nabla \cdot \mathbf{N}_i$$

Where: c_i = Concentration of the i^{th} species in the electrolyte [mol/m³]

\mathbf{N}_i = mass transport vector [mol/(m²*s)]

t = time [t]



This 2D Axisymmetric Electrodeposition Model:

Governing Processes: Nernst-Planck Equation

The electroneutrality condition is given as follows:

$$\sum_i z_i c_i = 0$$

Where: z_i = Charge of the i^{th} species in the electrolyte [1] (unitless)
 c_i = Concentration of the i^{th} species in the electrolyte [mol/m³]



This 2D Axisymmetric Electrodeposition Model:

Governing Processes: Butler-Volmer Equation {4}

The boundary conditions at the anode and the cathode are determined by the assumed electrochemical reaction and the Butler-Volmer equation.

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The assumed electrochemical reactions by which copper deposits on the cathode are as follows. (There are actually two reactions that occur.)

They are: $\text{Cu}^{2+} + e^- = \text{Cu}^+$ and $\text{Cu}^+ + e^- = \text{Cu}$.

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(Typically, since not all things are equal and it is known that the Rate Determining Step (RDS) (slowest) is the $\text{Cu}^{2+} + e^- = \text{Cu}^+$, by about a factor of 1000 {5}.)

It is also herein assumed that the $\text{Cu}^{2+} + e^- = \text{Cu}^+$ step is in equilibrium.

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Governing Processes: Butler-Volmer Equation {4}

That being the case, then the cathode mass transport is:

$$N_{Cu^{2+}} \cdot n = \frac{i_0}{2F} \exp\left[-\frac{1.5F\eta_{cat}}{RT}\right] \frac{c_{Cu^{2+}}}{c_{Cu^{2+},ref}} \exp\left[-\frac{0.5F\eta_{cat}}{RT}\right]$$

Where: N_i = mass transport vector [mol/(m²*s)]

n = normal vector

i_0 = Exchange current density [A/m²]

R = Universal gas constant [J/(mol*K)]

$c_{Cu^{2+}}$ = Concentration of the Cu²⁺ species in the electrolyte [mol/m³]

$c_{Cu^{2+},ref}$ = Reference concentration of the Cu²⁺ species in the electrolyte [mol/m³]

η_{cat} = Cathode overpotential [V]

F = Faraday's constant [A*s/mol]

T = Temperature [K]

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Governing Processes: Butler-Volmer Equation {4}

It then follows that, the anode mass transport is:

$$N_{Cu^{2+}} \cdot n = \frac{i_0}{2F} \exp\left[-\frac{1.5F\eta_{an}}{RT}\right] \frac{c_{Cu^{2+}}}{c_{Cu^{2+},ref}} \exp\left[\frac{0.5F\eta_{an}}{RT}\right]$$

Where: N_i = mass transport vector [mol/(m²*s)]

n = normal vector

i_0 = Exchange current density [A/m²]

R = Universal gas constant [J/(mol*K)]

$c_{Cu^{2+}}$ = Concentration of the Cu²⁺ species in the electrolyte [mol/m³]

$c_{Cu^{2+},ref}$ = Reference concentration of the Cu²⁺ species in the electrolyte [mol/m³]

η_{an} = Anode overpotential [V]

F = Faraday's constant [A*s/mol]

T = Temperature [K]

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Governing Processes: Butler-Volmer Equation {4}

For the insulating boundaries, where the mass transport is zero:

$$N_{Cu^{2+}} \cdot \mathbf{n} = 0$$

Where: $N_{Cu^{2+}}$ = mass transport vector [mol/(m²*s)]

\mathbf{n} = normal vector

A 2D Axisymmetric Electrodeposition Model

This 2D Axisymmetric Electrodeposition Model:

Governing Processes: Butler-Volmer Equation {4}

For sulfate ions, the insulating condition applies everywhere, thus:

$$N_{SO_4^{2+}} \cdot \mathbf{n} = 0$$

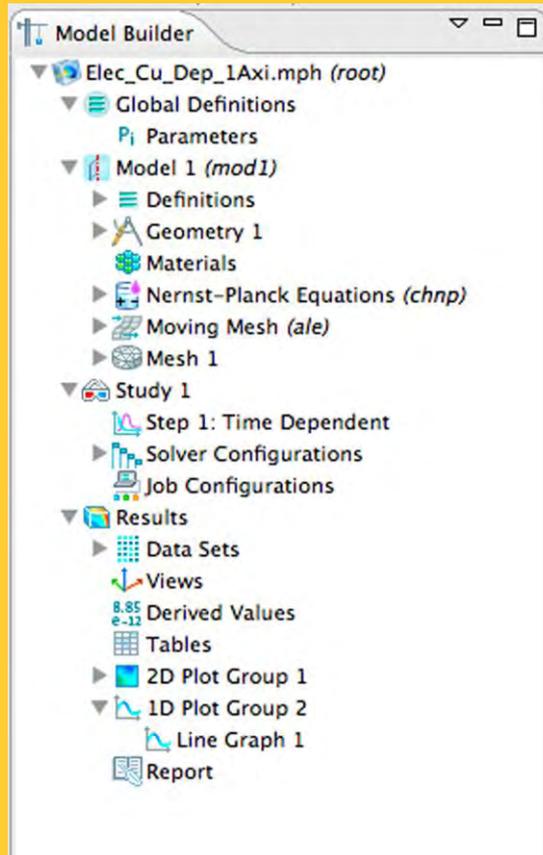
Where: $N_{SO_4^{2+}}$ = Mass Transport Vector [mol/(m²*s)]
 \mathbf{n} = normal vector

A 2D Axisymmetric Electrodeposition Model

This 2D Axisymmetric Electrodeposition Model:

Building the 2D Axisymmetric Electrodeposition Model

Model Builder Chart



A 2D Axisymmetric Electrodeposition Model

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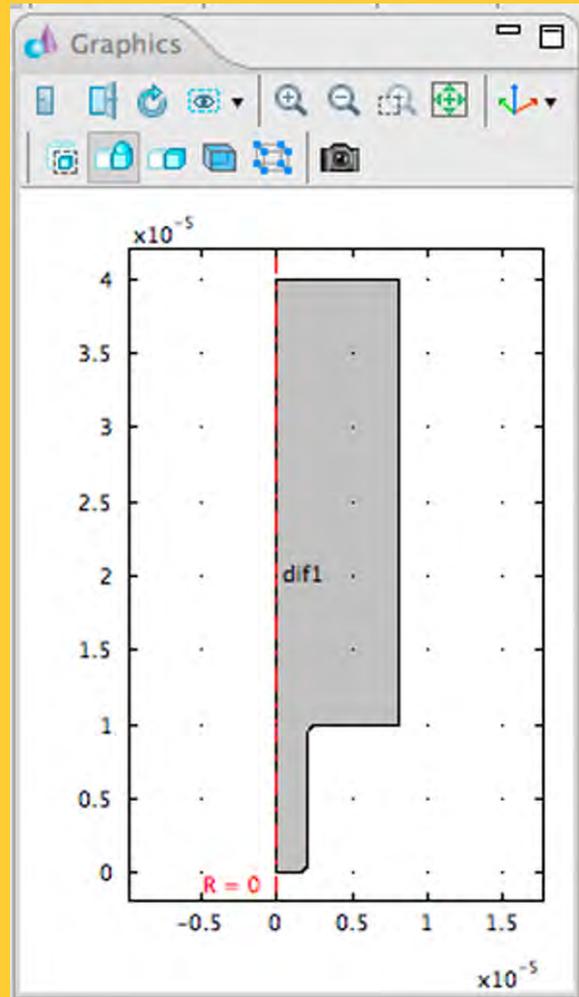
Global Parameters

| Name | Expression | Description |
|---------------|------------------------------|--------------------------------|
| Cinit | 500 [mol/(m ³)] | Initial concentration |
| T0 | 298[K] | System temperature |
| i0 | 150[A/m ²] | Exchange current density |
| phi_eq | 0[V] | Relative equilibrium potential |
| alpha | 0.75[1] | Symmetry factor |
| phi_s_anode | 0.0859[V] | Anode potential |
| phi_s_cathode | -0.0859[V] | Cathode potential |
| z_net | 2[1] | Net species charge |
| z_c1 | z_net[1] | Charge, species c1 |
| z_c2 | -z_net[1] | Charge, species c2 |
| um_c1 | D_c1/R_const/T0 | Mobility, species c1 |
| um_c2 | um_c1 | Mobility, species c2 |
| MCu | 63.546e-3[kg/mol] | Cu molar mass |
| rhoCu | 7.7264e3[kg/m ³] | Cu density |
| D_c1 | 2e-9[m ² /s] | Diffusivity |
| alpha1 | 0.5[1] | Symmetry factor |
| alpha2 | 1.5[1] | Diffusivity |
| D_c2 | D_c1 | Symmetry factor |

A 2D Axisymmetric Electrodeposition Model

This 2D Axisymmetric Electrodeposition Model: Building the 2D Axisymmetric Electrodeposition Model

Model Geometry

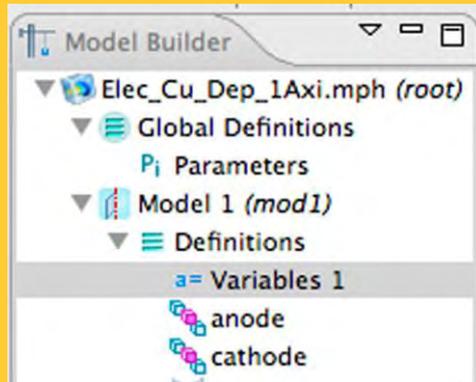


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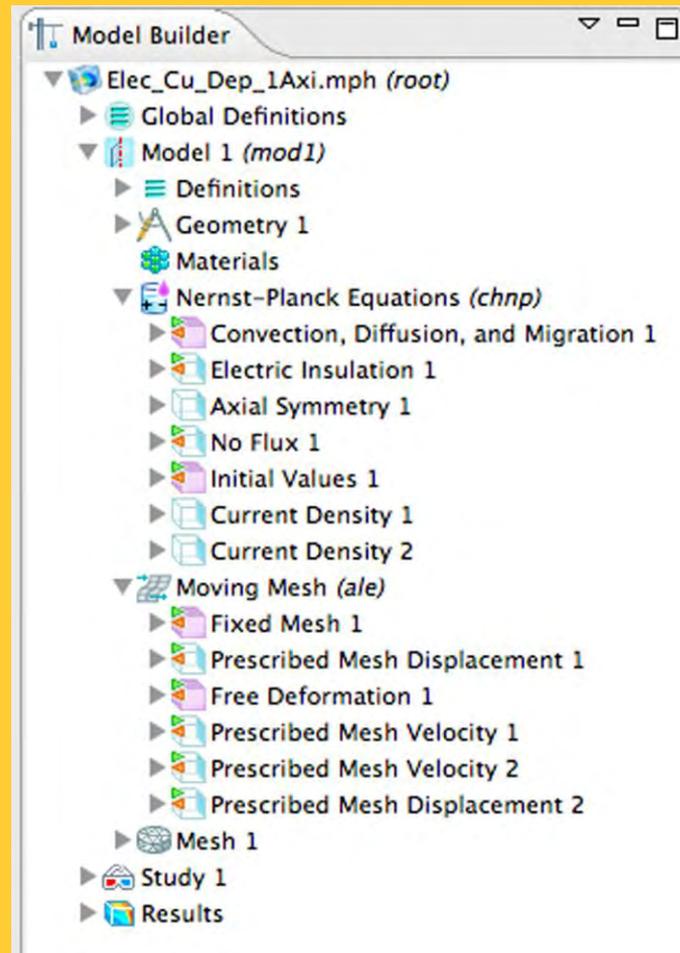
Local Variables



| Name | Expression | Description |
|-----------|---|--------------------------------------|
| i_anode | $i_0 * (\exp(\alpha * z_{net} * F_{const} / R_{const} / T_0 * (\phi_{s_anode} - V - \phi_{eq})) - c_1 / C_{init}) * \exp(-\alpha_1 * z_{net} * F_{const} / R_{const} / T_0 * (\phi_{s_anode} - V - \phi_{eq}))$ | Anode current density |
| i_cathode | $i_0 * (\exp(\alpha_2 * z_{net} * F_{const} / R_{const} / T_0 * (\phi_{s_cathode} - V - \phi_{eq})) - c_1 / C_{init}) * \exp(-\alpha_1 * z_{net} * F_{const} / R_{const} / T_0 * (\phi_{s_cathode} - V - \phi_{eq}))$ | Cathode current density |
| growth | $i_{cathode} * M_{Cu} / \rho_{Cu} / z_{net} / F_{const}$ | Deposition rate, cathode |
| n_growth | $i_{anode} * M_{Cu} / \rho_{Cu} / z_{net} / F_{const}$ | Deposition rate, anode |
| displ_r | $\text{abs}(r - R)$ | Absolute displacement in r direction |

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Domain and Boundary Specifications

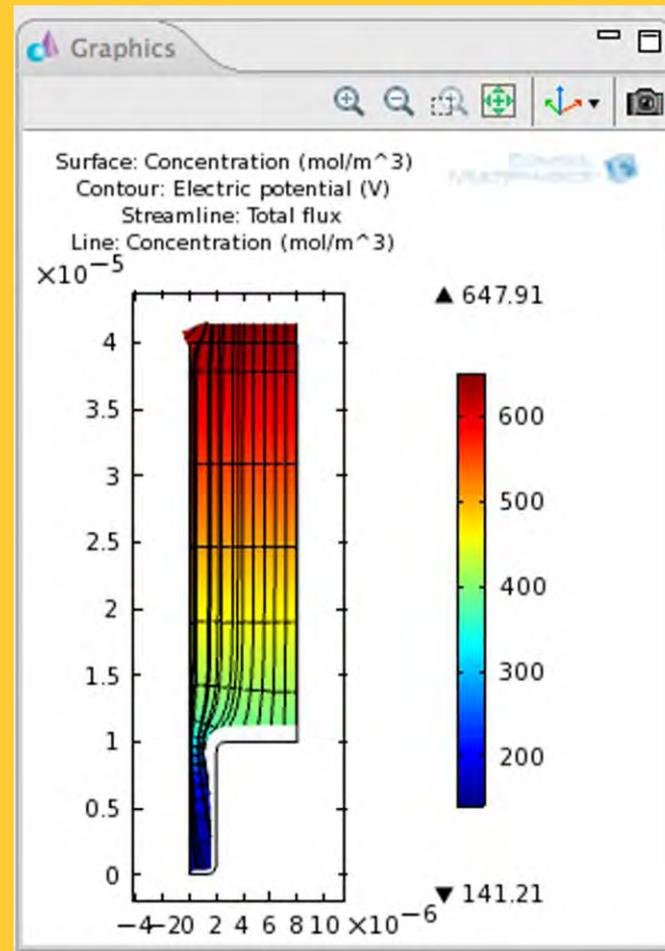


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This 2D Axisymmetric Electrodeposition Model:

Results

**Converged
Model**

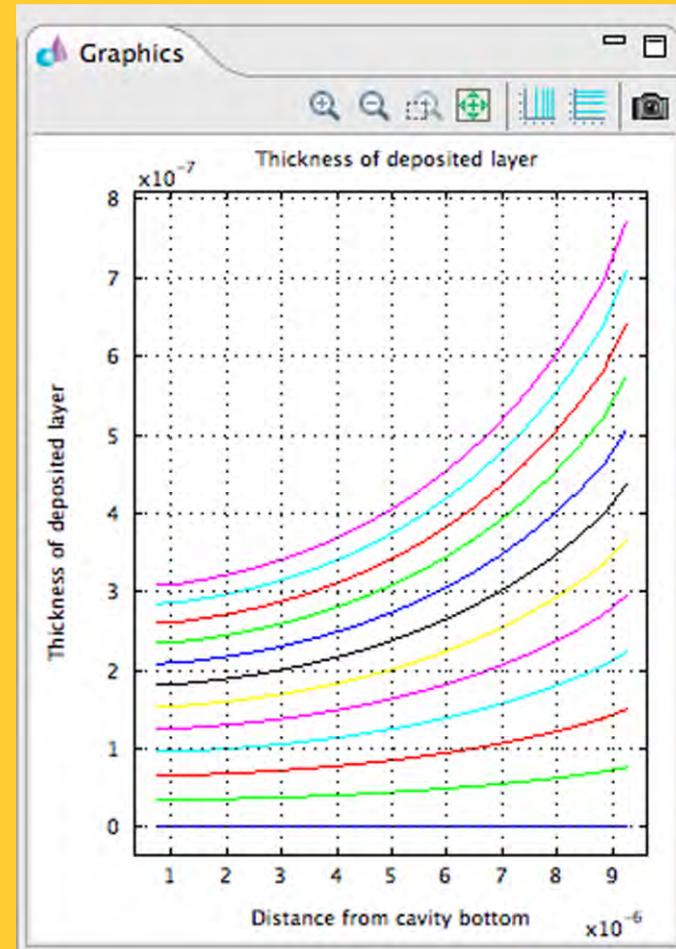


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Results

Electrodeposition Thickness



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Conclusions

COMSOL Multiphysics 4.x works well for the modeling of electrodeposition problems.

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References

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Thank You!